Dynamic load of the carrying structure of an articulated wagon with new draft gear concepts

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Abstract. The article deals with a new draft gear concept proposed by the authors to reduce the dynamic load of wagons in operational modes. The peculiarity of the concept is transformation of the kinetic impact energy into the work of viscous resistance forces when the viscous fluid passes through the throttle openings of the piston. The concept can be introduced for the wagons, in which centre sills of the frames are of closed sections. The mathematic modelling was conducted for the dynamic load of articulated wagons with consideration of the draft gear concept. It was established that the use of the draft gear concept can lower the dynamic load of wagons by about 10 %. The research will encourage engineers to design modern structures of rolling stock units and increase their operational efficiency.

Keywords: articulated wagon, carrying structure, dynamics, strength, transport mechanics.

1. Introduction

The competitive environment in the transportation market requires introduction of innovative engineering solutions to keep the leading position for the railway industry. Higher operational efficiency of the railway transport can be achieved by introduction of articulated wagons. The special feature of such wagons is the two-section carrying structure rested on three bogies. Such wagons have a number of considerable advantages in comparison with one-section ones; among them are lower production costs, lower vertical load on the frames, fewer number of required rolling stock units, etc.

Introduction of new innovative solutions in terms of the structure is essential for designing modern articulated wagons. It allows engineers to decrease the material capacity of wagons' carrying structures, and, respectively, the production costs.

Possible improvements of the technical and economic characteristics for railway vehicles are considered in [1]. But the study does not consider possible measures to decrease the dynamic load of wagons. The structural analysis of the innovative rolling stock manufactured at UralVagonZavod is made in [2]. The study considers modernization of rolling stock units and their components for higher operational efficiency. The measures for decreasing the dynamic load of the carrying structure of wagons under shunting impacts are not considered.

The structural analysis of BCNHL freight wagons is given in [3]. The study outlines possible ways to improve the technical and economic parameters of wagons for higher operational efficiency. The results of the structural and element analysis of a freight wagon are presented in [4]. The calculation was made with the finite element method. The research is conducted by an example of a BOXN25 open wagon used by Indian Railways. Determination of the dynamic load of wagons and techniques for its decrease under shunting impacts are not considered in the studies.

The dynamic load of articulated wagons is determined in [5, 6]. The special feature of such wagons is circular-pipe structural elements. The values of dynamic load, obtained through mathematic modelling, are considered in the strength calculation for the carrying structures of wagons, but the measures to decrease the dynamic load of the carrying structure of wagons are not considered.

Prospects of implementation of new-generation materials in the railway wagon production are presented in [7]. The study recounts some advantages of magnesium alloys used in the carrying systems of wagons. However, the article does not cover peculiarities of the dynamic load of wagons produced of such materials under operational modes.

The structural peculiarities of a long-base flat wagon are presented in [8]. The wagon has no frame-long centre sill, which is a special feature. The results of the strength calculation for the carrying structure of a flat wagon presented were realized in ANSYS software.

It should be mentioned that the design of the carrying structure of wagons considers the normative load values. Thus, the authors do not set the task to determine the dynamic load of the carrying structure of the wagon.

The objective of the study is determination of dynamic loads on the carrying structure of a circular-pipe wagon with consideration of the new draft gear concept instead of the automatic coupler CA-3. To achieve the objective, the following tasks were set:

- to propose techniques for lower dy11namic load on articulated wagons in operation;

- to conduct the mathematic modelling of dynamic loads on the carrying structure of an articulated wagon of circular pipes.

2. New draft gear concept for decreasing the dynamic load

The authors proposed a draft gear concept for decreasing the dynamic load of wagons under operational modes (Fig. 1).

Fig. 1. The draft gear concept of an automatic coupler a) the concept's components b) location on the wagon frame 1 – automatic couplers frame, 2 – wedge, 3 – adapter, 4 – circular-pipe centre sill, 5 – bottom, 6 – spring, 7 – telescopic element

The kinetic impact energy is transformed into the work of viscous energy forces. The resistance appears when the piston transfers the viscous liquid through the throttle openings by the operational principle of a hydraulic damper. The system returns to its initial state with the release spring in the telescopic element.

It should be mentioned, that such a draft gear concept can be used for railway vehicles with closed-section centre sills. This engineering solution can be used, e.g. for wagons with carrying elements of circular pipes (see Fig. 2).

The dynamic load of the carrying structure of the wagon with the draft gear concept was determined due to a mathematic functional notation of the process of dynamic load under the longitudinal force on the front draft gear stop (tension – jerk). The calculation was conducted by an example of an articulated flat wagon as one of the most popular types of articulated wagons in operation.

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Fig. 2. The spatial computer models of freight wagons: a) flat wagon, b) open wagon, c) boxcar, d) hopper wagon

The design diagram is presented in Fig. 3.

Fig. 3. The design diagram of an articulated flat wagon

$$
M'_{w} \cdot \ddot{x}_{w_{1}} + M_{W_{1}} \cdot h \cdot \ddot{\varphi}_{W_{1}} + k' (x_{w_{1}} - x_{w_{2}}) = P_{n} - \beta \cdot \dot{x}_{w_{1}},
$$

\n
$$
I_{w_{1}} \cdot \ddot{\varphi}_{w_{1}} + M_{W_{1}} \cdot h \cdot \ddot{x}_{w_{1}} - g \cdot \varphi_{w_{1}} \cdot M_{W_{1}} \cdot h
$$
\n(1)

$$
\begin{aligned} \n\mu_{1} & \mu_{W_{1}} \cdots \mu_{W_{1}} \mu_{W_{1}} \cdots \mu_{W_{1}} \mu_{W_{1}} \cdots \mu_{W_{1}} \mu_{W_{1}} \cdots \mu_{W_{1}} \mu_{W_{
$$

$$
M_{w_1} \cdot \ddot{z}_{w_1} = k_1 \cdot \Delta_1^{W_1} + k_2 \cdot \Delta_2^{W_1} - F_{FR} \left(sign \dot{\Delta}_1^{W_1} - sign \dot{\Delta}_2^{W_1} \right),
$$

\n
$$
m_i \cdot \ddot{x}_{w_1} + (m_i \cdot z_{c_i}) \cdot \ddot{\phi}_{w_1} = 0,
$$
\n(3)

$$
m_i \cdot \ddot{x}_{w_1} + (m_i \cdot z_{c_i}) \cdot \ddot{\varphi}_{w_1} = 0,
$$

\n
$$
I_i \cdot \ddot{\varphi}_{w_1} + (m_i \cdot z_{c_i}) \cdot \ddot{x}_{w_1} - g(m_i \cdot z_{c_i}) \cdot \varphi_{w_1} = 0,
$$
\n(4)

$$
m_i \cdot \ddot{z}_{w_1} = 0,
$$

\n
$$
M'_{w_2} \cdot \ddot{x}_{w_2} + M_{W_2} \cdot h \cdot \ddot{\varphi}_{w_2} - k' (x_{w_1} - x_{w_2}) = 0,
$$
\n(6)

$$
M'_{w_2} \cdot \ddot{x}_{w_2} + M_{W_2} \cdot h \cdot \ddot{\varphi}_{W_2} - k' (x_{w_1} - x_{w_2}) = 0,
$$

\n
$$
I_{w_2} \cdot \ddot{\varphi}_{w_2} + M_{W_2} \cdot h \cdot \ddot{x}_{w_2} - g \cdot \varphi_{w_2} \cdot M_{W_2} \cdot h
$$
\n(7)

$$
\mu_2 + \mu_2 + \cdots + \mu_2 = 0 \quad \text{(8)}
$$
\n
$$
= l \cdot F_{FR} \left(sign \Delta_1^{W_2} - sign \Delta_2^{W_2} \right) + l \left(k_1 \cdot \Delta_1^{W_2} - k_2 \cdot \Delta_2^{W_2} \right),\tag{8}
$$

$$
M_{w_2} \cdot \ddot{z}_{w_{22}} = k_1 \cdot \Delta_1^{W_2} + k_2 \cdot \Delta_2^{W_2} - F_{FR} \left(sign \dot{\Delta}_1^{W_2} - sign \dot{\Delta}_2^{W_2} \right),
$$

\n
$$
m_i \cdot \ddot{x}_{w_2} + (m_i \cdot z_{c_i}) \cdot \ddot{\varphi}_{w_2} = 0,
$$
\n(10)

$$
m_i \cdot \ddot{x}_{w_2} + (m_i \cdot z_{c_i}) \cdot \ddot{\varphi}_{w_2} = 0,
$$

\n
$$
I_i \cdot \ddot{\varphi}_{w_2} + (m_i \cdot z_{c_i}) \cdot \ddot{x}_{w_2} - g(m_i \cdot z_{c_i}) \cdot \varphi_{w_2} = 0,
$$
\n(10)

$$
m_i \cdot \ddot{z}_{w_2} = 0,\tag{12}
$$

where $\Delta_1^i = z_{w_1} - l \cdot \varphi_{w_1}, \Delta_2^i = z_{w_2} + l \cdot \varphi_{w_2}, M'_{Wi}$ – gross mass of the *i*-th section of a flat wagon;

 M_{Wi} – mass of the carrying structure of the *i*-th section of a flat wagon; I_{Wi} – inertia moment of the *i*-th section of a flat wagon; P_n – longitudinal force on the automatic coupler; β – viscous resistance coefficient formed by the draft gear concept; l – half-base of a flat-wagon section; F_{FR} $-$ absolute value of the dry force in a spring group; k' – rigidity of connection between the sections; k_1, k_2 – rigidities of the springs in the spring group of a flat wagon bogie (of Model 18-100); m_i – container mass; z_{ci} – height of the container's gravity centre; I_i – inertia moment of the *i*-th container; x_i , φ_i , z_i – coordinates corresponding to displacements of the flat wagon sections relative to the appropriate axles.

The research was conducted in the plane coordinates. The sections were elastically interacted. The longitudinal load on the carrying structure of a flat wagon was taken equal to 2.5 MN [9, 10]. The initial displacements and speeds were taken equal to zero [11-16]. Differential Eq. (1-12) were solved in MathCad environment by the Runge-Kutta method [17-23].

The results of the calculation showed than the accelerations on the carrying structure of the first section of a flat wagon from the force action, were 34.9 m/s², and on the second section – 34.2 m/s^2 (Fig. 4). The viscous resistance coefficient formed by the draft gear concept should exceed 70 kN/s∙m.

Fig. 4. The accelerations on the carrying structure of an articulated flat wagon a) the first section of a flat wagon from the longitudinal force, b) the second section of a flat wagon from the longitudinal force

Thus, the use of the draft gear concept for an articulated flat wagon makes it possible to reduce the dynamic load by about 10 %.

The calculations were also made for other types of articulated wagons of circular pipes. The numerical values of accelerations are given in Table 1.

of an articulated wagon of circular pipes		
Wagon type	Accelerations on the first	Accelerations on the second
	section from the force action	section from the force action
Open wagon	28.3	27.9
Boxcar	25.7	25.2
Hopper wagon		28.

Table 1. The numerical values of accelerations on the carrying structure of an articulated wag

The research conducted proved the efficiency of the draft gear concept for railway vehicles.

3. Conclusions

The authors proposed a draft gear concept for lower dynamic load of wagons under operational modes. This concept can be used for wagons with closed-section centre sills.

The study deals with the mathematical modelling of the dynamic load on the carrying structure

of an articulated flat wagon of circular pipes. The results of the calculation showed that the accelerations on the carrying structure the first section of a flat wagon from the action force were 34.9 m/s², and on the second section – 34.2 m/s².

It was established that the use of the draft gear concept for articulated wagons can help decrease the dynamic load by about 10 %.

The research will encourage engineers to design modern structures for railway vehicles of better operational efficiency.

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