

Influence of installation deviation on dynamic performance of synchronous magnetic coupling

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Received 7 May 2017; accepted 8 May 2017

DOI <https://doi.org/10.21595/vp.2017.18600>



Abstract. To improve dynamic characteristics of synchronous magnetic coupling, this paper mainly analyzed the influence of the installation deviation on the synchronous magnetic coupling's dynamic performance used in the horizontal axis wave energy power generation device. Dynamic characteristics equations based on Lagrange equation are built in the paper to analyze the dynamic characteristic of synchronous magnetic coupling. The radial deviation, the angle deviation and the center-of-mass deviation are considered in the equation. The influence of those installation deviations on the synchronous magnetic coupling performance is analyzed based on the mathematical model. The results show that the rise time, the overshoot, the peak time, the adjusting time and the oscillation of the synchronous magnetic coupling are almost not affected by those installation deviations.

Keywords: synchronous magnetic coupling, dynamic performance, installation deviation.

1. Introduction

Synchronous magnetic coupling has many characteristics, including isolated transmission, flexible transmission, overload protection, as shown in Fig. 1. It is widely applied to places require to be completely sealed or isolated from the vibration of the input. Sometimes it is used to avoid overloading [1-3]. It can be used in many devices, such as wave energy device, wind equipment [4]. In addition to these advantages, the synchronous magnetic coupling has a low request for the installation precision and it is convenient to fix and use.

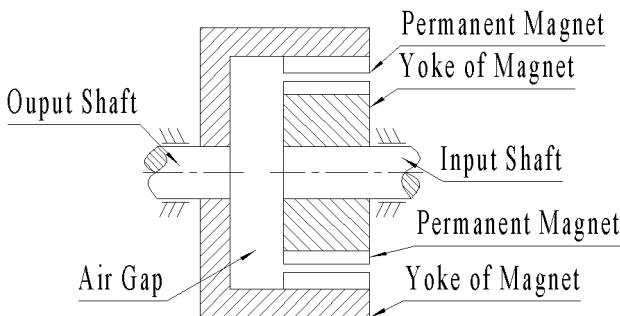


Fig. 1. Synchronous magnetic coupling

The horizontal axis wave energy power generation device is the floating type wave energy device. It works in bad sea condition. It is very hard to maintain. So, the device requires high reliability. For the marine equipment, one of the most common problems is seawater infiltration. The equipment will suffer great destruction that can make the equipment lose working ability and scrapped. During two sea trials, the horizontal axis wave energy power generation device suffered seawater infiltration in different degrees. Analysis found that the location at the connective part

between the water turbine and the coupling was radial contact seal. The radial contact seal failed. Seawater entered into the device continuously. And as time went on, seawater accumulated and the device finally lost working ability. By searching papers, magnetic drive mechanism used in the chemical pump was introduced into the horizontal axis wave energy power generation device. It can achieve zero leakage of the seal unit at the transmission part and improve the device reliability.

This paper mainly analyzed the influence of the installation deviation on synchronous magnetic coupling performance used in the horizontal axis wave energy power generation device. The device captured wave energy and then converted it into turbine rotational mechanical energy. The speeder accelerated the turbine and drove the generator. The compartment setting speeder needs to be isolated from the seawater and is protected from seawater infiltration. The sealing reliability requirement is very high. So, the synchronous magnetic coupling is used as torque transmission mechanism.

It was difficult to ensure coaxiality between the speeder and the water turbine because the horizontal axis wave energy power generation device size is 6 m×6 m×6 m, which is large. The water turbine's diameter is 1.5 m, and its length is 4 m. Fig. 2 is the prototype device. Fig. 3 is the device schematic diagram. The traditional transmission mechanism often uses rigid connection. There is a big prestressing force after installation if there is the installation error. That creates the pulsating stress in the transmission part when the device works. It accelerates the failure of the device. The synchronous magnetic coupling can solve a series of problems caused by the installation error at the transmission position. And it allows the position deviation. In order to analyze the influence of the installation deviation on synchronous magnetic driver performance, the research is carried out.



Fig. 2. Prototype device

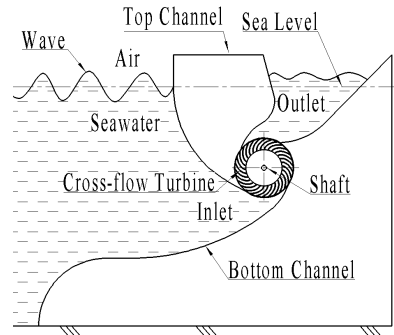


Fig. 3. Device schematic diagram

2. Mathematical model

The synchronous magnetic coupling performance is influenced by magnet parameters, air-gap, load [5]. There's installation deviations when the synchronous magnetic coupling is installed. The installation error may be axial, radial or angle direction, as shown in Fig. 4. In order to analyze the influence of the installation deviation on synchronous magnetic coupling performance, the driven rotor installation deviations are analyzed.

Lagrange equation is usually used to build dynamic equations of mechanism [6-8], it can analyze the dynamic characteristics by defining generalized force and generalized coordinates. The dynamic equations deduced from Lagrange equation can avoid constraint reaction and reduce solving difficulty.

The Lagrange equation is written as:

$$\frac{d}{dt} \left(\frac{\partial(T - U)}{\partial \dot{q}_j} \right) - \frac{\partial(T - U)}{\partial q_j} = Q_j, \quad (1)$$

where q_j is generalized coordinates; \dot{q}_j is generalized velocity; T is kinetic energy; U is potential energy; Q_j is generalized force.

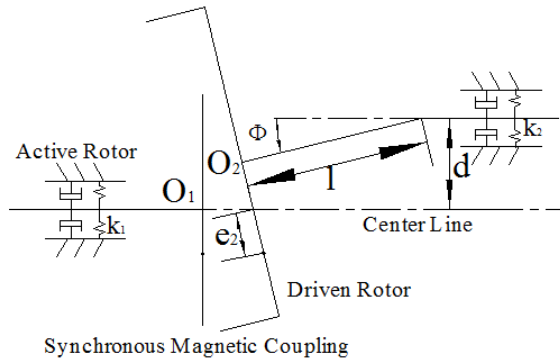


Fig. 4. Installation deviation

According to geometric relations and Fig. 4, The kinetic energy T is:

$$T = \frac{1}{2}J_1\dot{\theta}_1^2 + \frac{1}{2}(J_2 + m_2e_2^2)\dot{\theta}_2^2 + \frac{1}{2}m_1v_{c1}^2 + \frac{1}{2}m_2v_{c2}^2, \quad (2)$$

where m_1 is the mass of the active rotor; m_2 is the mass of the driven rotor; v_{c1} is translational velocity of the active rotor; v_{c2} is the translational velocity of the driven rotor; J_1 is the rotational inertia of the active rotor; J_2 is the rotational inertia of the driven rotor; e_1 is the center-of-mass deviation of the active rotor; e_2 is the center-of-mass deviation of the driven rotor; θ_1 is the rotation angle of the active rotor; θ_2 is the rotation angle of the driven rotor.

The potential energy U is:

$$U = \frac{1}{2}k\Delta\theta^2 + \frac{1}{2}k_1(x_1^2 + y_1^2) + \frac{1}{2}k_2(x_2^2 + y_2^2), \quad (3)$$

where k_1 is the elastic stiffness of input; k_2 is the elastic stiffness of output; $\Delta\theta$ is angular difference between the active and driven rotors; k is the torsional rigidity; (x_2, y_2) are the geometric center coordinates O_2 of the driven rotor; (x_1, y_1) are the geometric center coordinates O_1 of the active rotor.

The input torque T_1 and damping force $c_1\dot{\theta}$ are applied on the active rotor, as the damping force $c_2\dot{\alpha}$ are applied on the driven rotor. Those torques and forces are non-potential generalized force, so:

$$Q_j = \begin{bmatrix} T_1 - c_1\dot{\theta} \\ -c_2\dot{\alpha} \end{bmatrix}. \quad (4)$$

According to Eqs. (1-4), dynamic equations of synchronous magnetic coupling can be expressed as:

$$m_2[d + l\sin(\Phi)]\{-\sin(\theta_2)\ddot{x}_1 - \cos(\theta_2)\dot{\theta}_2\dot{x}_1 + \cos(\theta_2)\ddot{y}_1 - \sin(\theta_2)\dot{\theta}_2\dot{y}_1 + [d + l\sin(\Phi)]\ddot{\theta}_2\} + m_2e_2^2\ddot{\theta}_2 + J_2\ddot{\theta}_2 - k(\theta_1 - \theta_2) + k_2[d + l\sin(\Phi)][\cos(\theta_2)\dot{\theta}_2y_1 - \sin(\theta_2)\dot{\theta}_2x] = -c_2\dot{\theta}_2. \quad (5)$$

Because the geometric center coordinates O_1 is fixed, dynamic equations can be simplified as follows:

$$\{m_2[d + l\sin(\Phi)]^2 + m_2e_2^2 + J_2\}\ddot{\alpha} - k(\theta_1 - \theta_2) = -c_2\dot{\theta}_2. \quad (6)$$

The transfer function $G(s)$ between θ_1 and θ_2 is got from Eq. (6):

$$G(s) = \frac{k}{\{m_2[d + l\sin(\Phi)]^2 + m_2e_2^2 + J_2\}s^2 + c_2s + k} \quad (7)$$

3. Dynamic characteristics analysis

According to the measurement and calculation, $J_2 = 0.17 \text{ Kg}\cdot\text{m}^2$, $C_2 = 1.37 \text{ Nm}\cdot\text{s}/\text{rad}$, $k = 45 \text{ Nm}/\text{rad}$, $m_2 = 6.5 \text{ Kg}$, $l = 0.1 \text{ m}$. Then the influence of the center-of-mass deviation e_2 , radial deviation d and angle deviation Φ on the dynamic characteriare is analyzed.

According to physical measurement, the diameter of the driven rotor is 160 mm, so e_2 is set as 0, 5, 10, 15, 20 mm to analyze the unit step dynamic response characteristic of the synchronous magnetic coupling. The Dynamic Response Curve of e_2 is obtained, as shown in Fig. 5. From Fig. 5, rise time, peak time and accommodation time are almost unchanged with the increase of the center-of-mass deviation e_2 . The maximum overshoot and oscillation times keep unchange with various center-of-mass deviation e_2 . So, the center-of-mass deviation e_2 has little influence on the dynamic characteristic of the synchronous magnetic coupling.

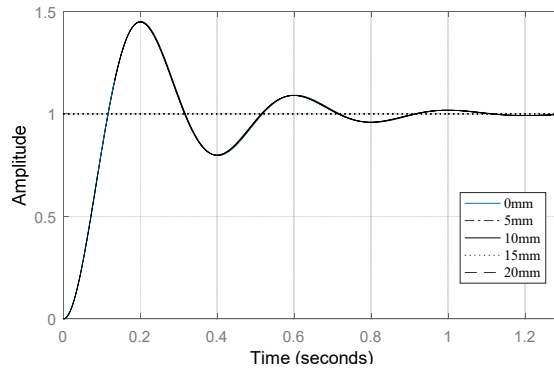


Fig. 5. Dynamic response curve of e_2

The air gap between the driven rotor and the active rotor is 6 mm, so d is set as 0, 1.5, 3, 4.5, 6 mm to analyze the unit step dynamic response characteristic of the synchronous magnetic coupling. The Dynamic Response Curve of d is obtained, as shown in Fig. 6. According to Fig. 6, radial deviation d has almost no effect on dynamic characteristic like the center-of-mass deviation e_2 .

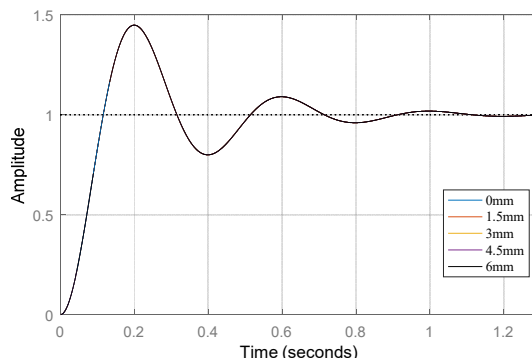


Fig. 6. Dynamic response curve of d

The length of the driven rotor is 50 mm, and the air gap is 6 mm, so Φ is set as 0, 0.03, 0.06, 0.09, 0.12 rad to analyze the unit step dynamic response characteristic of the synchronous magnetic coupling. The Dynamic Response Curve of Φ is obtained, as shown in Fig. 7. The angle deviation Φ has almost no effect on dynamic characteristic like the radial deviation d and the center-of-mass deviation e_2 .

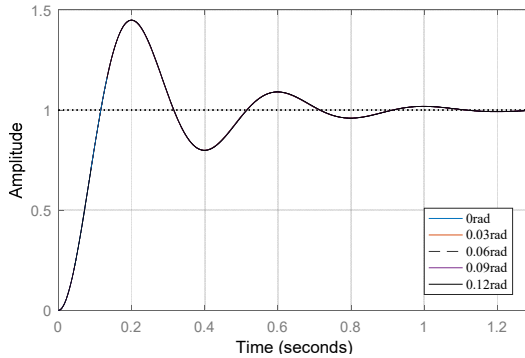


Fig. 7. Dynamic response curve of Φ

According to the above analysis, the center-of-mass deviation e_2 , radial deviation d and angle deviation Φ have almost no effect on the dynamic characteristics of the synchronous magnetic coupling. When the installation deviations exist, the synchronous magnetic coupling can work as no installation deviations. That means the synchronous magnetic coupling is a flexible transmission mechanism and allows the installation deviations exists in the horizontal axis wave energy power generation device.

4. Conclusions

According to the analysis mentioned above, the dynamic characteristics of the synchronous magnetic coupling is almost not effected by the installation deviations, including the center-of-mass deviation e_2 , radial deviation d and angle deviation Φ . The analysis results show that the synchronous magnetic coupling is a flexible transmission mechanism and can improve the dynamic characteristics with the installation deviations. The synchronous magnetic coupling can be used in the wave energy power generation device to improve the device reliability and practicality and avoid the influence of installation deviations on the device performance.

Acknowledgements

The research is supported by the Fundamental Research Funds of Shandong University (Project No. 2016JC035) and the Natural Science Foundation of Shandong Province (Project No. ZR2016WH02), which are gratefully acknowledged.

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